

## Elastic Snap-Through Instabilities Are Governed by Geometric Symmetries

Basile Radisson and Eva Kanso

*Department of Aerospace and Mechanical Engineering, University of Southern California, Los Angeles, California 90089-1191, USA*

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Many elastic structures exhibit rapid shape transitions between two possible equilibrium states: umbrellas become inverted in strong wind and hopper popper toys jump when turned inside out. This snap through is a general motif for the storage and rapid release of elastic energy, and it is exploited by many biological and engineered systems from the Venus flytrap to mechanical metamaterials. Shape transitions are known to be related to the type of bifurcation the system undergoes, however, to date, there is no general understanding of the mechanisms that select these bifurcations. Here we analyze numerically and analytically two systems proposed in recent literature in which an elastic strip, initially in a buckled state, is driven through shape transitions by either rotating or translating its boundaries. We show that the two systems are mathematically equivalent, and identify three cases that illustrate the entire range of transitions described by previous authors. Importantly, using reduction order methods, we establish the nature of the underlying bifurcations and explain how these bifurcations can be predicted from geometric symmetries and symmetry-breaking mechanisms, thus providing universal design rules for elastic shape transitions.

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Bistability and snap-through transitions are key phenomena in many biological [1,2] and manmade [3,4] systems. Bistability refers to a system with two stable equilibrium states. Snap through occurs when a system is in an equilibrium state that becomes unstable or suddenly disappears, as a control parameter is varied. Familiar examples range from the Venus flytrap [1] to children's toys [3] and ancient catapults [5]. Mechanical metamaterials, whose behavior is governed by their geometric structure rather than elastic properties, can be designed to exploit these instabilities to induce shape transitions and switch between multiple modes of functionality [6].

Elastic strips of length  $L$ , whose ends are first brought together by a distance  $\Delta L$  to cause the strip to buckle into one of two stable shapes [Fig. 1(a), movie S1 in the Supplemental Material [7]], then driven by boundary actuation, provide an intuitive system to demonstrate shape transitions (Figs. 1 and 2, movies S2 and S3 [7]) [4,8]. Starting from the Euler-buckled strip with clamped-clamped (CC) boundary conditions (BCs), when both ends are rotated symmetrically and held at a nonzero angle  $\alpha$ , one equilibrium takes an “inverted” shape while the other maintains its “natural” shape. A larger rotation causes the inverted shape to snap to the natural shape. Rotating only one end also creates a violent snap through, albeit of different character [4]. A clamped-hinged (CH) strip with the hinged end free to rotate in place and the clamped end sheared by a distance  $d$  in the direction transverse to the buckled shape exhibits snap through [8]. A similar setup with CC BCs leads to graceful merging of the two equilibrium states.

Despite the relative simplicity of realizing these transitions experimentally [4,8], an understanding of how shape transitions are selected remains lacking. In a beautiful analysis, [4] showed that snap through in asymmetric BCs arises from a saddle-node bifurcation and argued that in the case of symmetric BCs, it results from a subcritical pitchfork bifurcation, without explaining what leads to this change in the character of the bifurcation as BCs change. In [8], the authors alluded to similarities between their system and that of [4]. However, to date, no general theory exists for designing systems that achieve or avoid a specific type of transition. Here, we combine numerical and analytical methods to reveal the mechanisms governing shape transitions in boundary-actuated elastic strips, and we prove that the two systems in [4,8] are equivalent. Importantly, to predict the type of bifurcation and establish design rules for creating a desired shape transition, we show that these transitions are governed by geometric symmetries.

Symmetry is one of the most fundamental concepts in physics. Symmetries shape the energy landscape and govern the equilibrium configurations the system can adopt. Broken symmetries are often invoked to explain transitions in a range of physical systems from condensed matter physics [16] to quantum field theory [17], turbulence theory [18], fluid dynamics [19], biological locomotion [20,21], and combustion phenomena [22]. Simple one-dimensional (1D) examples from bifurcation theory show that a broken symmetry can turn a graceful pitchfork bifurcation into a violent saddle-node bifurcation (Supplemental Material [7], Sec. S1), [9]. Extending this understanding to infinite-dimensional systems is challenging to researchers

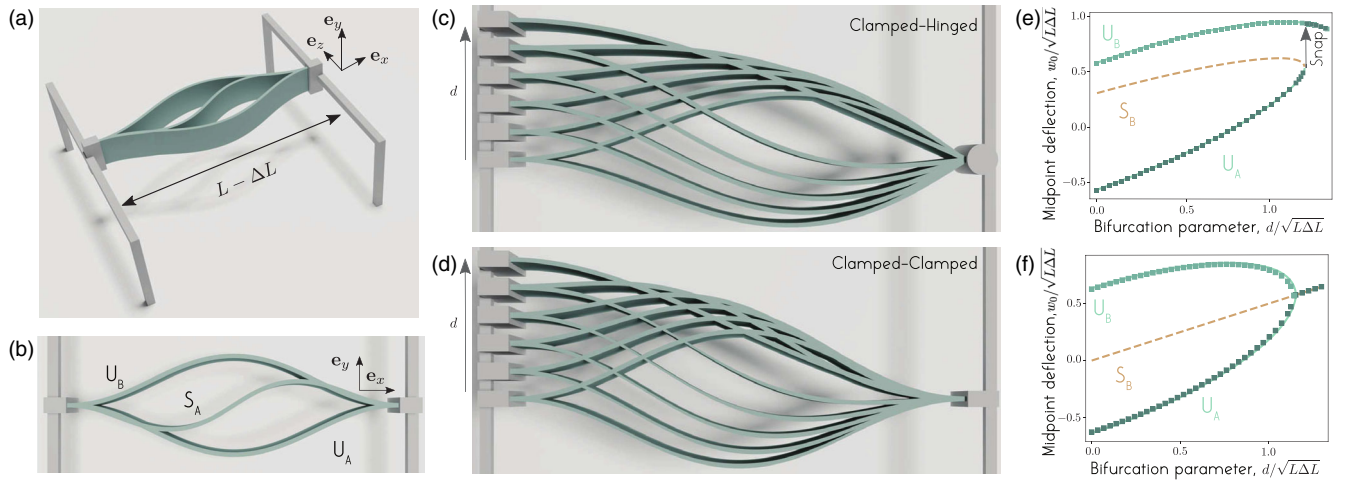


FIG. 1. (a),(b) Elastic buckled strip with clamped-clamped boundary conditions exhibits two symmetric stable equilibria  $U_A$  and  $U_B$ , and pairs of unstable equilibria of alternating symmetry at increasing energy levels,  $S_A$  and  $S_B$  denoting the first unstable pair ( $S_B$  not shown). [(c)–(f)] Actuation of buckled strip by (quasistatically) translating its left end by a distance  $d$  leads to loss of bistability and a shape transition that depends on BCs: (c),(e) CH strip exhibits a violent snap through, (d),(f) the transition in the CC strip is smooth. [(a)–(d)] 3D computer graphics rendering of the Cosserat numerical simulations. (e),(f) Midpoint deflection  $w/\sqrt{L\Delta L}$  versus bifurcation parameter  $d/\sqrt{L\Delta L}$ . In all figures, (green) square markers represent data obtained based on the Cosserat rod theory. Solid (green) and dashed (brown) lines represent, respectively, stable and unstable branches obtained from the Euler beam model.

and educators alike. The understanding we develop for elastic strips could thus serve as an educational tool to illustrate the role of symmetry breaking in the bifurcation of continuum systems.

We investigate the bifurcation behavior of the elastic strips introduced in [4,8] numerically (Figs. 1 and 2), by leveraging the three-dimensional (3D) Cosserat theory [23], and its discrete counterpart, the discrete elastic rod

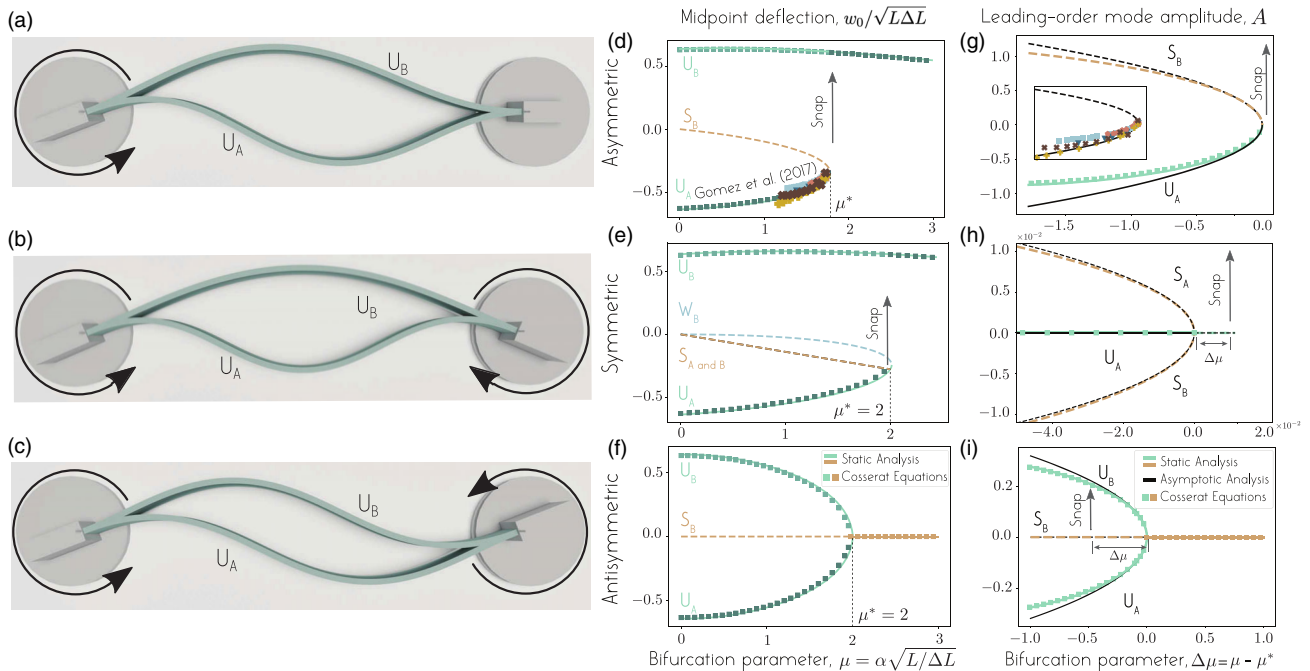


FIG. 2. Boundary actuation and bifurcation diagrams from (quasistatically) rotating one or both clamped ends in (a) asymmetric, (b) symmetric, and (c) antisymmetric fashion. [(d)–(f)] Midpoint deflection as a function of bifurcation parameter  $\mu = \alpha\sqrt{L}/\Delta L$ . Experimental data from [4] are superimposed. [(g)–(i)] Asymptotic analysis near the bifurcation point  $\mu^*$  gives access to normal forms describing the amplitude  $A(t)$  of the leading order mode. Bifurcation diagrams of the normal forms (black lines) agree quantitatively with data obtained from the Euler beam equations (green and brown lines) and Cosserat simulations (green and brown square markers), and experimental data.

[10] (Supplemental Material [7], Sec. S2). To establish bifurcation diagrams and carry out asymptotic analysis, we also analyze the strip's behavior in the limit of small deflection  $w(x, t)$ , with  $-L/2 < x < L/2$ , based on the Euler-Bernoulli Beam theory ([3,4], and Supplemental Material [7], Sec. S2),

$$\rho b h \frac{\partial^2 w}{\partial t^2} + B \frac{\partial^4 w}{\partial x^4} + F \frac{\partial^2 w}{\partial x^2} = 0. \quad (1)$$

The material properties of the strip are denoted by  $\rho$  (density),  $b$  (width),  $h$  (thickness), and  $B = E b h^3 / 12$  (bending stiffness, with  $E$  the Young's modulus). The applied compressive load is denoted by  $F$ . In this limit, the inextensibility condition gives rise to the nonlinear constraint equation

$$\int_{-L/2}^{L/2} \left( \frac{\partial w}{\partial x} \right)^2 dx = 2\Delta L. \quad (2)$$

The Euler-buckled strip [Figs. 1(a) and 1(b)] admits an infinite family of static equilibria that come in pairs, ordered by increasing value of elastic bending energy  $\mathcal{E}_b$  (Supplemental Material [7], Sec. S4). We refer to members of the same pair as *twin solutions*. The fundamental buckling mode, i.e., lowest energy level, corresponds to two stable  $U$ -shape equilibria ( $U_A$  and  $U_B$ ). Higher modes are unstable and alternate between odd and even harmonics. The first unstable mode gives rise to a twin of  $S$ -shape equilibria labeled  $S_A$  and  $S_B$ .

Through systematic numerical experiments, we investigate how boundary actuation modifies the  $U_A$  and  $U_B$  equilibria. In Fig. 1, we control the transverse distance  $d$  at the clamped end of the CH and CC strip (Supplemental Material [7], Sec. S5). In Fig. 2, we control the rotation at one or both ends of the CC strip by specifying the tangent direction (angle  $\alpha$ ) at the boundaries (Supplemental Material [7], Sec. S6). The control parameters are varied incrementally starting from the twin solutions  $U_{A,B}$ , allowing the elastic strip to reach mechanical equilibrium at each increment. In Figs. 1(e), 1(f), and 2(d)–2(f), we plot the strip's midpoint deflection  $w$ , normalized by the length scale  $\sqrt{L\Delta L}$ , as a function of the nondimensional control parameters  $d/\sqrt{L\Delta L}$  and  $\alpha\sqrt{L/\Delta L}$ , respectively. Bistability is lost beyond a certain threshold in all cases, but the character of this transition depends on boundary actuation. Asymmetric and symmetric rotations cause snap through from the inverted ( $U_A$ ) to the natural ( $U_B$ ) shape, as does transverse shearing of the CH strip. The dynamic evolution of the strip differs during snapping: the displacement of the midpoint grows quadratically in time in the asymmetric case, while it grows exponentially in time in the symmetric case [11]. Antisymmetric rotations and transverse shearing of the CC strip induce graceful merging of the equilibrium shapes  $U_{A,B}$ . These findings are

consistent with experimental observations [4,8], and agree quantitatively with [4].

To understand the mechanisms leading to the similarities and differences in these shape transitions, we solved Eqs. (1)–(2) to arrive at analytic expressions for the infinite set of twin equilibria for each type of boundary actuation, and we assessed their linear stability subject to small perturbations (Supplemental Material [7], Sec. S2–S5). This analysis matches quantitatively the numerical solutions in Figs. 1(e), 1(f), and 2(d)–2(f) for small  $\Delta L$ , and shows that, depending on the type of boundary actuation, the stable equilibrium  $U_A$  that is energetically unfavored by the boundary actuation must collide with one or both unstable  $S_{A,B}$  equilibria at the shape transition.

Importantly, the similarity of the bifurcation diagrams in Figs. 1 and 2 is not a coincidence. We proved, by introducing a frame of reference attached to the line connecting the strip's end points, that transverse shearing of the strip is equivalent to rotation of its boundaries (Supplemental Material [7], Sec. S8). Hereafter, we use the strip actuated by rotating its endpoints, with  $\mu = \alpha\sqrt{L/\Delta L}$  as the bifurcation parameter, when discussing geometric symmetries and the role they play in selecting the type of bifurcation underlying a shape transition.

So which symmetries matter? Three symmetries are important and best introduced in the context of the Euler-buckled strip at  $\mu = 0$ : top-bottom reflection ( $w \rightarrow -w$ ), left-right reflection ( $x \rightarrow -x$ ), and  $\pi$  rotation ( $w \rightarrow -w$  and  $x \rightarrow -x$ ). Equations (1)–(2) are invariant under all three transformations (Supplemental Material [7], Sec. S3). Because the state of the system is infinite dimensional, we calculate the bending energy  $\mathcal{E}_b = (EI/2) \int_{-L/2}^{L/2} (\partial^2 w / \partial x^2)^2 dx$  at  $U_{A,B}$  and  $S_{A,B}$  and depict the energy landscape semischematically on a reduced 2D space consisting of the deflection  $w$  evaluated at the strip's mid and quarter length [Fig. 3(a); Supplemental Material [7], Sec. S10]. In Fig. 3(b), we unfold the energy landscape along the closed black curve connecting the  $U$  and  $S$  shapes. This representation highlights two important properties at  $\mu = 0$ : the minimum energy barrier—difference in  $\mathcal{E}_b$  between  $S_{A,B}$  and  $U_{A,B}$ —that the strip needs to overcome in order to undergo a shape transition from  $U_A$  to  $U_B$ , and the geometric symmetries that map  $U_A$  to  $U_B$  and  $S_A$  to  $S_B$ , and vice versa. Specifically, the left-right symmetry maps each  $U$  solution to itself and the top-bottom and  $\pi$ -rotation symmetries map a  $U$  solution to its twin, whereas the  $\pi$ -rotation symmetry maps each  $S$  solution to itself and the top-bottom and left-right symmetries map an  $S$  solution to its twin. Hereafter, we refer to the  $\pi$  rotation that maps the  $U$ -twin shapes to one another as the *U-twin symmetry* and the left-right reflection that maps the  $S$ -twin shapes to one another as the *S-twin symmetry*. The type of shape transition the system undergoes for  $\mu \neq 0$  is directly related to which twin symmetry gets broken by boundary actuation.

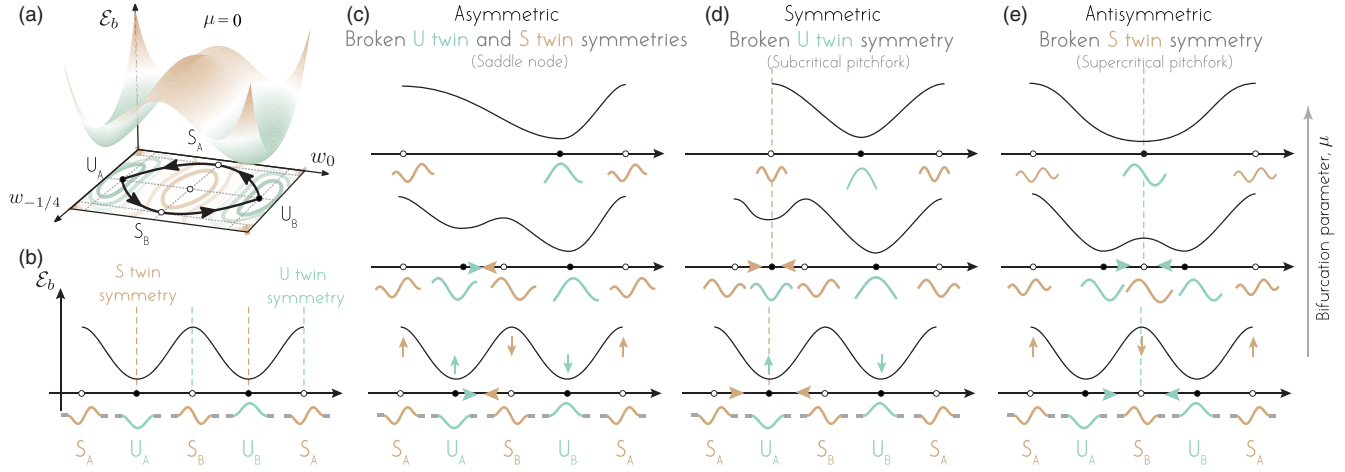


FIG. 3. (a) Energy landscape at  $\mu = 0$ : two potential wells at the two stable equilibria  $U_{A,B}$  separated by lowest energy barriers at the first pair of unstable equilibria  $S_{A,B}$ . The two paths connecting  $U_A$  to  $U_B$  via either  $S_A$  or  $S_B$  constitutes the energetically cheapest routes to pass from  $U_A$  to  $U_B$ . (b) 1D periodic representation of energy landscape. [(c)–(e)] Rotating one or both of the boundaries reshapes the energy landscape: breaking both  $U$ - and  $S$ -twin symmetries leads to a saddle-node bifurcation; breaking either  $U$ - or  $S$ -twin symmetry leads to a pitchfork bifurcation.

Asymmetric boundary actuation breaks both  $U$ - and  $S$ -twin symmetries. It requires  $U_A$  to bend more than  $U_B$  and  $S_A$  to bend more than  $S_B$ , thus increasing the bending energy of  $U_A$  and  $S_A$  and decreasing that of  $U_B$  and  $S_B$  [Fig. 3(c)]. This causes  $U_A$  and  $S_B$  to monotonically approach each other until they merge and suddenly vanish. The system must jump to  $U_B$ . Symmetric actuation breaks the  $U$ -twin symmetry but conserves the  $S$ -twin symmetry. It requires  $U_A$  to bend more than  $U_B$  but it equally affects  $S_A$  and  $S_B$ . Thus,  $S_A$  and  $S_B$  remain energetically equivalent while the energetic state of  $U_A$  increases and approaches that of  $S_A$  and  $S_B$  until they all merge in a single unstable equilibrium [Fig. 3(d)], leaving the system no option but to jump to  $U_B$ . Antisymmetric actuation conserves the  $U$ -twin symmetry but not the  $S$ -twin symmetry:  $U_A$  and  $U_B$  remain energetically equivalent while  $S_A$  bends more than  $S_B$ ;  $U_A$  and  $U_B$  monotonically approach  $S_B$  until they all gracefully merge in a single stable equilibrium [Fig. 3(e)].

This intuitive understanding of geometric symmetries is substantiated by extending the asymptotic analysis of [4] to derive normal forms near the shape transition at  $\mu^*$ . We set  $\mu = \mu^* + \Delta\mu$  with  $\Delta\mu \ll 1$ , and introduce the dimensionless variables  $X = x/L$ ,  $W = w/\sqrt{L\Delta L}$ ,  $W_{\text{eq}}^* = w_{\text{eq}}^*/\sqrt{L\Delta L}$ ,  $T = t\sqrt{B/\rho b h L^4}$  and  $\Lambda^2 = FL^2/B$ . To analyze the dynamic of the strip near the bifurcation, we define a slow timescale  $\tau = \Delta\mu^a T$ , and expand the dynamic state of the strip in powers of  $\Delta\mu$  [4,11],

$$\begin{aligned} W(X, \tau) &= W_{\text{eq}}^*(X) + \Delta\mu^b W_0(X, \tau) + \text{h.o.t.}, \\ \Lambda(\tau) &= \Lambda_{\text{eq}}^* + \Delta\mu^c \Lambda_0(\tau) + \text{h.o.t.} \end{aligned} \quad (3)$$

Here, the values of  $a$ ,  $b$ , and  $c$  depend on the intrinsic properties of the system. In [11], we present a systematic

approach to calculate them. We find that, for the asymmetric BCs,  $a = 1/4$ ,  $b = c = 1/2$  as postulated in [4], whereas for the symmetric and antisymmetric BCs,  $a = b = 1/2$ , and  $c = 1$ . We substitute  $a$ ,  $b$ , and  $c$  into (3) and write  $\Delta\mu^b W_0 = A(T)\Phi_0(X)$ , where  $\Phi_0(X)$  is the shape of the leading order mode and  $A(T)$  its unscaled amplitude. We arrive at a reduced form for each boundary actuation (see Ref. [11]). For the asymmetric BCs, the normal form obtained in [4] is representative of a saddle node bifurcation

$$\frac{d^2 A}{dT^2} = a_{1,\text{asym}} \Delta\mu + a_{2,\text{asym}} A^2, \quad (4)$$

where  $a_{1,\text{asym}}$  and  $a_{2,\text{asym}}$  are positive constants (explicit expressions in [4,11]). For the symmetric and antisymmetric BCs, we obtain a normal form representative of a pitchfork bifurcation (explicit expressions of  $b_{1,(.)}$  and  $b_{2,(.)}$  in [11]),

$$\frac{d^2 A}{dT^2} = b_{1,(.)} \Delta\mu A + b_{2,(.)} A^3. \quad (5)$$

For the symmetric case, the coefficients  $b_{1,\text{sym}}$  and  $b_{2,\text{sym}}$  are positive, and the cubic term is destabilizing (subcritical pitchfork), whereas for the antisymmetric case, the coefficients  $b_{1,\text{anti}}$  and  $b_{2,\text{anti}}$  are negative and the cubic term is stabilizing (supercritical pitchfork).

Bifurcation analysis of (4) and (5) recapitulates the results in Fig. 3. For  $\Delta\mu < 0$ , (4) admits a stable equilibrium (representing  $U_A$ ) and an unstable equilibrium (representing  $S_B$ ) that collide and annihilate at  $\Delta\mu = 0$  [Fig. 2(g)]. As  $U_A$  vanishes, the strip is forced to snap to  $U_B$  (not represented in the reduced form). For  $\Delta\mu < 0$ , (5) admits three equilibria. In the symmetric case, these



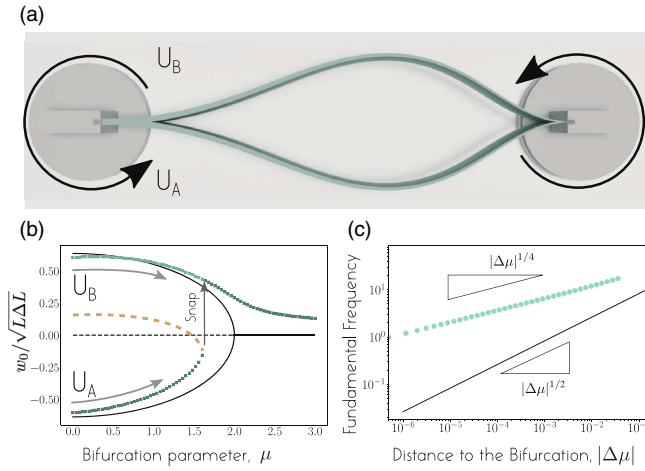


FIG. 4. (a) Tapered elastic strip under antisymmetric boundary rotation. (b) Midpoint deflection (green symbols) versus bifurcation parameter exhibits snap through as opposed to the graceful merging of a homogeneous strip subject to the same actuation (black lines). (c) Critical slowing down near the bifurcation scales as  $(\Delta\mu)^{1/4}$  as in the case of a saddle node.

equilibria represent  $U_A$ ,  $S_A$ , and  $S_B$ , that merge at  $\Delta\mu = 0$  [Fig. 2(h)].  $U_A$  becomes unstable and the strip is forced to snap to  $U_B$ . In the antisymmetric case, the three equilibria represent  $U_A$ ,  $U_B$ , and  $S_B$ . They merge at  $\Delta\mu = 0$  [Fig. 2(i)]. The simultaneous shape change from  $U_A$  and  $U_B$  to  $S_B$  is graceful.

To quantitatively compare this asymptotic analysis to the data in Figs. 2(d) and 2(e), we calculated the amplitude  $A$  directly from data (Supplemental Material [7], Sec. S9) and plotted the results in Figs. 2(g)–2(i) as a function of the distance from the bifurcation  $\Delta\mu$ , measured from the respective  $\mu^*$  value. We observe good agreement (near  $\mu^*$ ) with the bifurcation diagrams of the normal forms (black lines). Notably, the reduced forms capture correctly, not only the static shape bifurcations, but also the dynamics of snapping near these bifurcations [4,11].

The normal forms in (4) and (5) provide the backbone for plotting schematically the energy landscapes in Figs. 3(d)–3(f), which exhibit all the features of the rigorous bifurcation analysis (Supplemental Material [7], Sec. S10). Importantly, the well-known symmetry breaking mechanism that turns a pitchfork into a saddle node bifurcation [9] (Supplemental Material [7], Sec. S1), appears here, in an infinite dimensional system, governing elastic transitions. This intuitive yet universal understanding of elastic instabilities based on symmetries of the Euler-buckled strip provides powerful tools for diagnostics and design. It helps explain the force hysteresis observed in [8] (Supplemental Material [7], Sec. S7). It can also help design programmable metamaterials with tunable bistability and rapid (algebraic or exponential) actuation capabilities. For a buckled elastic strip, clamped at both ends and driven via antisymmetric rotations, to undergo a nonlinear snap

through, we must break the  $U$ -twin symmetry. This can be achieved by using a strip with geometric or material heterogeneity, such as a geometrically tapered strip instead of a homogeneous strip (Fig. 4, Supplemental Material [7], Sec. S11). Future work will consider extensions of this analysis to elastic shells and origami-based structures [24].

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